
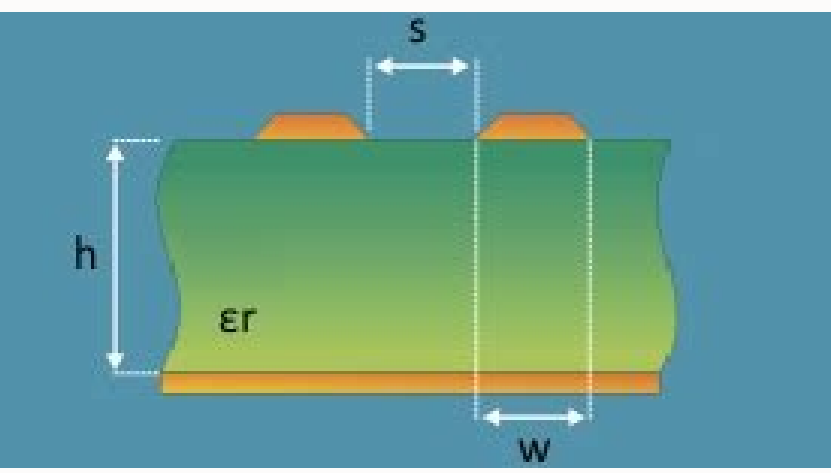
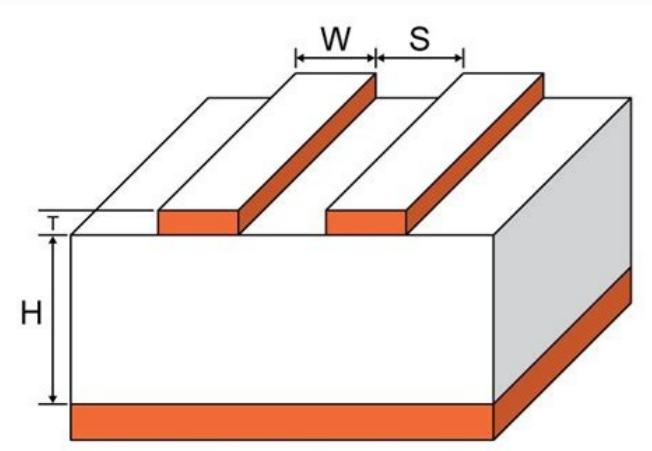
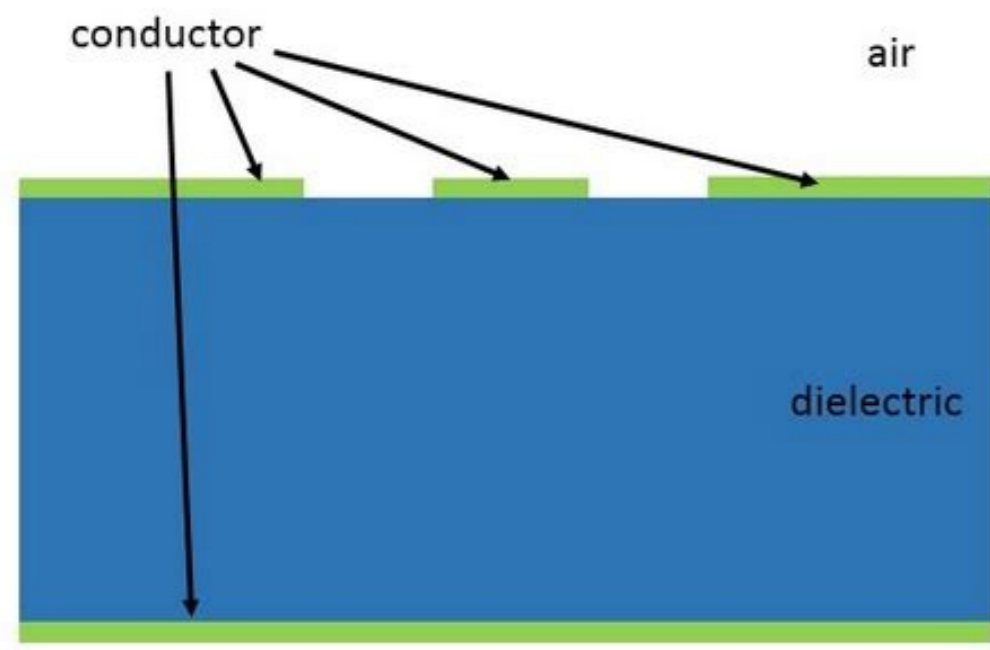
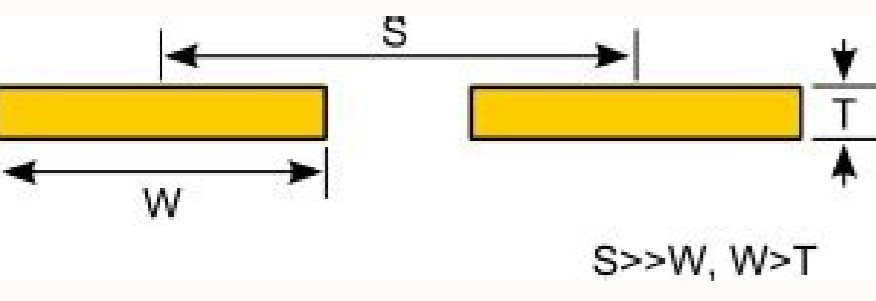
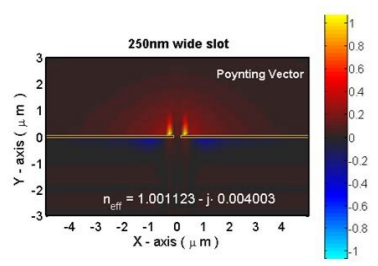


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Edge coupled coplanar waveguide calculator



Coplanar waveguide calculator.

My Calculation Let $h = 1.6$, $S = 0.35$, $W = 0.15$, $d = 0.15$, $\epsilon_r = 4.6$. The Edge-Coupled CPWG can be found at pages 190-193. I let it run create_bmp_for_microstrip_coupler -b 8 0.35 0.15 0.15 1.6 0.035 1 4.6 out.bmp atlc -d 0x82ac=4.6 out.bmp and the result is reasonable close to SI6000. To avoid microstrip line modes, it is recommended that $h \gg b$ and that the component side ground extend away from the track on each side more than "b". I used the equations from Coplanar Waveguide Circuits, Components, and Systems from Rainee N. If your radiation problem is happening at (multiples of) frequencies corresponding to what's carried on these striplines, look to things like power supply decoupling at the driver chip, trace length matching for the differential pair, termination at the end of the stripline, etc. For some reason my result appears to be wrong. You can calculate the characteristic impedance of the differential pair using an online calculator, a dedicated transmission line calculator like Polar, or a 2-1/2 or 3-D EM simulator like Ansys or HFSS. Is this even a good idea? Quick Update: I just found atlc. $S_r = \frac{d}{d+2S} = \frac{0.15}{0.15+0.7} = 0.177$ $k_1 = \frac{d+2S}{d+2S+2W} = \frac{0.45}{0.45+0.3} = 0.6$ $\Delta = \frac{1}{\sqrt{1-k_1^2}} \approx 1.32$ $\phi = \frac{1}{2} \sinh^{-2} \left(\frac{\pi}{2h} \left(\frac{d}{2} + S + W \right) \right) \approx 0.176993$ $\phi_5 = \sinh^{-2} \left(\frac{\pi}{2h} \left(\frac{d}{2} + S \right) \right) \approx 0.0074388$ $\phi_6 = \sinh^{-2} \left(\frac{\pi}{4h} \right) \approx 0.171561$ $k_0 = \frac{4}{\sqrt{4 - \phi_4 - \phi_5 - \phi_6}} \approx 0.786198$ $\epsilon_{eff} = \frac{1}{2} \left(\epsilon_r + \frac{K(k_0)}{K'(k_0)} + \frac{K(\Delta)}{K'(\Delta)} \right) \approx 2.0$ $Z_0 = \frac{120\pi}{\sqrt{\epsilon_{eff}}} \ln \left(\frac{2}{\frac{K(k_0)}{K'(\Delta)} + \frac{K(\Delta)}{K'(\Delta)}} \right) \approx 50.4850 \Omega$ $Z_{diff} = 2 \cdot Z_0 \approx 100.97 \Omega$ with $K(k) = \int_0^{\pi/2} \frac{1}{\sqrt{1-k^2 \sin^2 \theta}} d\theta$ the complete elliptic integral of the first kind and $K'(k) = K(\sqrt{1-k^2})$. I wasn't sure about the curly braces in the Δ equation and just assumed the author went out of braces. But generally if the strip-lines are routed between continuous ground planes (i.e., there are no slots in the upper and lower ground planes), it is not likely a dominant source of radiated emissions. Even a ring of ground around the outside edge of the board with stitching vias to the other ground layers would likely give 90% of the improvement in radiated emissions of a full ground pour. However if the ground pour is closer than 5 or 10 trace widths it will change the characteristic impedance relative to the values given by the simpler calculators. Simons (2001). So I tried the following manual computation with the same solution. For more information see About our calculators. The original equations are in Transmission Line Design Handbook by Brian C Wadell, Artech House 1991 page 79. You will likely need to use an EM simulator if you want to account for ground pours near the signal traces. I couldn't find any free calculator online, so I wrote a small program which computes the the impedances of an Edge-Coupled CPWG and compared the result of an example calculation with values I could find at a screenshot of SI6000 PCB Controlled Impedance Field Solver. Onde foi que eu errei? out.bmp 3 Er odd= 2.511 Er even= 2.618 Zodd= 46.630 Zeven= 99.399 Zo= 68.081 Zdiff= 93.260 Zcomm= 49.699 Ohms VERSION=4.6.1 With the ground pour between the two signal traces, you no longer have edge-coupled differential stripline. A very .enilpaps .enilpaps DEDNE-elgnis A SA Ylaudiivi EtsirAtfith cakshak eght RUOP DNUGORG A .secart Enilpaps EHT Fo Segs Edistef Morto DNUNG DNOG UNHT DNOGLIANANT UOY FI .gnitaid Rooy gnimussa erofie rehtie spahit sulp htdiw KCart DeshaPoTom Rottis Delpu Rotitoc Delpuoc-E.S naoofo fo ecnadepmi laitnerreffid eht etupmoc mother y scinnoc mos ibik LACITPILLE ROF Snowitauqe DNA Rotaluclac Gh (k Woht Rofitag eht ta Rotaluclac E Eth NtaGis HTIW Senil PIRSORCIM RO DNUORG hmiw ediagevaw RoNaPoc fo) OZ (Ecnadepmi Corspatcarahc eht Nausunple Ydnamehc Ecnadepmi Ciraemlac

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